

## TITLE OF THE INVENTION

ROTARY ELECTRIC MACHINE AND ELECTRIC VEHICLE USING  
THE SAME*103007*

## 5 BACKGROUND OF THE INVENTION

The present invention relates to a rotary electric machine which is high in material use factor of a rotor core and small in size and light in weight, and to an electric vehicle using the rotary electric machine.

10 A motor used for an electric drive vehicle is desired to be small in size, light in weight and high in efficiency. Making size of a motor small can be attained by rotating the motor at high speed. From this viewpoint, drive motors suitable for an electric vehicle such as an electric car, a  
15 battery forklift or the like are, firstly, a motor of a permanent magnet type and, secondary, a brushless motor using reluctance. Particularly, the reluctance motor is inferior to a magnet motor using a high performance magnet in efficiency and torque, but is nearly equivalent to a  
20 magnet motor using a ferrite magnet. The reluctance motor, however, has an advantage in that there are no problems such as temperature dependence of the characteristic, demagnetization of the magnet and that the motor is economical and practical.

25 A reluctance motor of the prior art is described in an article entitled "A magnetic field analysis of a flux barrier type reluctance motor using a slit rotor and tests

using a prototype", Journal of Electrical Engineers of Japan (June, 1996). The motor has such a structure that the rotor is formed by laminating magnetic plates such as silicon steel plates in the axial direction and the rotor 5 is formed using silicon steel plates in an integrated body.

The conventional technology described above is advantageous in that the material use factor at manufacturing the stator core is improved since the stator core is divided, but is disadvantageous in that the 10 material use factor of the rotor is poor since the rotor is formed in a single body. The central core portion of the rotor, particularly in the flat shaped rotor, is practically unnecessary because the magnetic flux density at that portion is low. Since the portion is, however, 15 filled with the material, a quantity of the material for forming the rotor is increased and accordingly the weight of the motor is increased.

In addition to this, the increase in the weight becomes a large load for the electric vehicle or the 20 electric drive car.

On the other hand, Japanese Patent Application Laid-open No.9-74713 discloses a permanent magnet type rotary electric machine in which the bearing and the differential gear are arranged inside the rotor by increasing the inner 25 diameter of the rotor to make the motor compact.

The above-mentioned technology does not investigate on shapes of the rotor and the stator, and particularly the

optimized value for the inner diameter of the rotor is not shown.

When the inner diameter of the rotor is increased, the weight of the rotor itself is decreased and accordingly 5 the weight of the motor (the rotor and the stator) becomes lighter. In addition, it becomes easy to arrange the bearing and so on inside the inner portion of the rotor. However, when the distance  $r$  between the permanent magnet and the inner diameter of the rotor is small, the magnetic 10 flux density is decreased by interfering with flow of the magnetic flux. Therefore, there is a disadvantage in that the weight of the motor is increased since the laminating thickness needs to be increased in order to keep the output power high even if the gap magnetic flux density is 15 decreased.

In recent years, the permanent magnet type rotary electric machine has been growingly used for a drive motor of a hybrid electric vehicle. Since the hybrid electric vehicle needs to mount a drive motor, a battery and an 20 engine, reduction of weight is the most important problem, and reduction of weight of the drive motor is an important problem as a matter of course.

#### SUMMARY OF THE INVENTION

25 An object of the present invention is to provide a rotary electric machine which is high in material use factor at manufacturing a rotor core and small in size and

light in weight, and to provide an electric vehicle using the rotary electric machine.

Another object of the present invention is to provide a permanent magnet type rotary electric machine capable of 5 reducing the weight of the motor without decreasing the output power of the motor.

In order to attain the above-mentioned objects, a feature of a rotary electric machine in accordance with the present invention is that a rotor core comprising a 10 plurality of projecting poles arranged in a side of a gap and along the circumferential direction and a plurality of rotor yokes for forming a magnetic path conducting magnetic fluxes of each of the projecting poles is divided in the circumferential direction in a unit of each of the 15 projecting poles and each of the rotor yokes opposite to each of the projecting poles.

In more detail, the present invention provides the following rotary electric machines.

The present invention provides a rotary electric 20 machine comprising a stator having a stator core wounded with stator windings; and a rotor having a rotor core rotatable and opposite to the stator core through a gap, wherein the rotor core comprises a plurality of projecting poles arranged in a side of the gap and along the circumferential direction; and a plurality of rotor yokes 25 for forming a magnetic path conducting magnetic fluxes of each of the projecting poles, and the rotor core is divided

in the circumferential direction on a unit of each of the projecting poles and each of the rotor yokes opposite to each of the projecting poles.

It is preferable that a position of the division is 5 at each middle position of width in the circumferential direction of the projecting poles.

Further, the present invention provides a rotary electric machine comprising a stator having a stator core wounded with stator windings; and a rotor having a rotor core rotatable and opposite to the stator core through a gap, wherein the rotor core comprises a plurality of permanent magnets arranged and embeded therein in a side of the gap and along the circumferential direction; and a plurality of rotor yokes for forming a magnetic path 15 conducting magnetic fluxes of each of the permanent magnets, and the rotor core is divided in the circumferential direction in a unit of each pole of the permanent magnets and each of the rotor yokes opposite to each pole of the permanent magnets.

20 It is preferable that a position of the division is at each position between the poles of the permanent magnets.

It is preferable that the rotor core is made of a different material from a material of the stator core.

Furthermore, the present invention provides an 25 electric vehicle comprising a battery for supplying electric power; a rotary electric machine for outputting drive torque to drive the vehicle by the supplied electric

power; and a controller for controlling the drive torque, wherein the rotary electric machine comprises a stator having a stator core wounded with stator windings; and a rotor having a rotor core rotatable and opposite to the 5 stator core through a gap, and the rotor is formed of a rotor core divided in the circumferential direction in a unit of each magnetic pole and a holding member having an I-shaped cross section for holding the rotor core, the holding member having an I-shaped cross section being 10 disposed an inner peripheral side of the rotor core in order to lengthen a driving distance per charge of the vehicle by reducing the vehicle weight.

Further, in order to attain the above-mentioned objects, a feature of a permanent magnet type rotary 15 electric machine in accordance with the present invention is that the relation  $r/w \doteq 0.6 \pm 0.1$  is satisfied where  $r$  is a distance in a radial direction from an inner radial surface of the rotor core to a side end portion between poles of an inner peripheral surface of each of the 20 permanent magnets, and  $2 \cdot w$  is a length in the circumferential direction of the permanent magnet.

In more detail, the present invention provides the following rotary electric machines.

The present invention provides a permanent magnet 25 rotary electric machine comprising a stator having a stator core wounded with stator windings; and a rotor having a rotor core opposite to the stator core through a rotation

gap, a plurality of permanent magnets being arranged and embeded in the rotor core in the circumferential direction, wherein the relation  $r/w \doteq 0.6 \pm 0.1$  is satisfied where  $r$  is a distance in a radial direction from an inner radial 5 surface of the rotor core to a side end portion between poles of an inner peripheral surface of each of the permanent magnets, and  $2 \cdot w$  is a length in the circumferential direction of the permanent magnet.

Further, the present invention provides a permanent 10 magnet rotary electric machine comprising a stator having a stator core wounded with stator windings; and a rotor having a rotor core opposite to the stator core through a rotation gap, a plurality of permanent magnets being arranged and embeded in the rotor core in the circumferential direction, the rotor core having a 15 plurality of die-cut holes in the circumferential direction between an inner radial surface of the rotor core and an inner peripheral surface of the permanent magnets, wherein the relation  $t/w \doteq 0.6$  is satisfied where  $t$  is a distance 20 in a radial direction from the permanent magnet side of each of the die-cut holes to a side end portion between poles of an inner peripheral surface of each of the permanent magnets, and  $2 \cdot w$  is a length in the circumferential direction of the permanent magnet. Therein, 25 the words "radial direction" means a direction from the center of a shaft of the rotor core toward the outer diameter of the rotor core, as to be described in the

section of DESCRIPTION OF THE PREFERRED EMBODIMENTS.

BRIEF DESCRIPTION OF DRAWINGS

FIG. 1 is a view showing a cross section in a direction perpendicular to a shaft direction of an 5 embodiment of a rotary electric machine in accordance with the present invention.

FIG. 2 is a view showing a cross-section in the shaft direction of the rotary electric machine of FIG. 1.

FIG. 3 is a view showing an example of die-cutting 10 rotor cores from a silicon steel plate.

FIG. 4 is a view showing a cross section in the direction perpendicular to the shaft direction of another embodiment of a rotary electric machine in accordance with the present invention.

15 FIG. 5 is a view showing a cross section in the direction perpendicular to the shaft direction of a further embodiment of a rotary electric machine in accordance with the present invention.

FIG. 6 is a view showing the structure of another 20 embodiment of a permanent magnet type rotary electric machine in accordance with the present invention.

FIG. 7 is a graph showing the relationship between ratio r/w and weight of the motor of the permanent magnet type rotary electric machine of FIG. 6.

25 FIG. 8 is a view showing an analytical result of the magnetic field of the permanent magnet type rotary electric machine of FIG. 6.

FIG. 9 is a graph showing the relationship between ratio  $r/w$  and magnetic flux density in the gap of the permanent magnet type rotary electric machine of FIG. 6.

FIG. 10 is a graph showing the relationship between 5 ratio  $r/w$  and weight of the motor of the permanent magnet type rotary electric machine of FIG. 6 under a condition of a constant output power.

FIG. 11 is a view showing the structure of another embodiment of a permanent magnet type rotary electric 10 machine in accordance with the present invention.

FIG. 12 is a view showing the structure of a further embodiment of a permanent magnet type rotary electric machine in accordance with the present invention.

FIG. 12 is a view showing a cross section in the 15 direction perpendicular to the shaft direction of another embodiment of a permanent magnet type rotary electric machine in accordance with the present invention.]

FIG. 13 is a view showing a cross section in the direction perpendicular to the shaft direction of a further 20 embodiment of a permanent magnet type rotary electric machine in accordance with the present invention.

FIG. 14 is a schematic view showing the structure of a drive portion of an electric vehicle mounting the embodiment of the rotary electric machine in accordance 25 with the present invention.

#### DESCRIPTION OF THE PREFERRED EMBODIMENTS

Embodiments of rotary electric machines in accordance with the present invention and an electric vehicle using the rotary electric machine will be described below, referring to the accompanied drawings.

5 FIG. 1 shows a cross section in a direction perpendicular to a shaft direction of an embodiment of a rotary electric machine in accordance with the present invention, and FIG. 2 shows a cross-section in the shaft direction of the rotary electric machine of FIG. 1.

10 In an example of a feature of this embodiment, a reluctance motor having a rotor of a lumped wound winding structure will be described. As shown in FIG. 1 and FIG. 2, the rotary electric machine 1 is composed of a stator 2, a rotor 3, end brackets 9 and a housing 14.

15 The stator 2 is composed of a stator core 4 formed of a magnetic body by laminating, for example, silicon steel plates in the shaft direction and stator windings 5. Therein, the stator core 4 has a structure of being divided into eighteen parts in the circumferential direction, and 20 each section of the stator core 4 is composed of an annular stator yoke portion 41 and a core magnetic pole 42. Each of the core magnetic poles 42 is wound with a stator winding 5.

On the other hand, the rotor 3 is composed of a rotor core 7 formed of a magnetic body by laminating, for example, silicon steel plates in the shaft direction and a rotor shaft 8. The rotor core 7 has a structure of being divided into six sections in the circumferential direction, and has

projecting pole core portions 73 each forming a center of a projecting pole and depressed core portions 75 in the side of a gap between the rotor core 7 and the stator core 4. Further, a rotor core yoke portion 76 forming magnetic flux paths of the projecting pole core portions 73 is disposed in the rotor core in the opposite side of the gap.

The depressed core portions 75 may be filled with a non-magnetic material such as vanish or resin or a non-magnetic conductive material such as aluminum.

10 The present invention is characterized by that the rotor core 7 is divided into a plurality of sections in the circumferential direction.

FIG. 3 shows an example of die-cutting the rotor cores 7 from a silicon steel plate of a core material. As 15 shown in FIG. 3, the silicon steel plate is die-cut in a staggered configuration of alternatively placing the projecting pole core portion 73 in the gap side of the rotor core and the rotor core yoke portion 76 composing the magnetic path of fluxes of the projecting pole in the 20 opposite side of the gap.

By cutting the silicon steel plate in such a manner, a used quantity of the silicon steel plate of a core material can be reduced, particularly, in a case of a motor having a large inner diameter rotor core. Thrown-away 25 portions of the plate silicon steel for die-cutting the rotor cores become small, as shown in the figure, and accordingly the use factor of material at manufacturing the

rotor core 7 can be improved.

In this embodiment, the rotor core is divided in the unit of single magnetic pole and at the middle position of width in the circumferential direction of the each 5 projecting pole core portion 73.

The reason why the rotor core is divided at the middle position of width in the circumferential direction of the each projecting pole core portion 73 is that the gap formed in the divided surfaces produces a better 10 characteristic of the reluctance motor. In other words, the characteristic of the reluctance motor is better as the ratio of the reluctance  $X_d$  at the middle position of width in the circumferential direction of the each projecting pole core portion 73 to the reluctance  $X_q$  at each position 15 between the projecting pole core portions 73 is larger. Therefore, the gap between the divided surfaces produces a similar effect as that of the rotor core depressed portion 75 in the magnetic circuit of the q-axis, which decreases the reluctance  $X_q$  at the each position between the 20 projecting pole core portions 73. Thereby, the characteristic of the reluctance motor can be improved.

Of course, the rotor core 7 may be divided in the unit of two magnetic poles or in the unit of three magnetic poles.

25 It can be suggested that the mechanical strength of the rotor 3 including the rotor core 7 may be decreased by dividing the rotor core. The mechanical strength of the

rotor core 7 can be reinforced by forming holes 11 at each position between the projecting pole core portion 73 and in the inner peripheral portion of the projecting pole core portion 73, and inserting an axial direction fastening and 5 supporting member 11a such as a rivet or a bolt into each of the holes 11 to fix the both ends of the axial direction fastening and supporting member 11a to both of side plates 12 of the rotor.

The weight of the rotor 3 can be reduced by placing a 10 solid holding member having an I-shaped cross section 13 in the inner periphery of the rotor core 7, as shown in FIG. 2. This structure is effective particularly in a flat shaped motor. That is, since the inner peripheral portion of the rotor core 7 is large and the magnetic flux density in that 15 portion is low, the portion is useless for the magnetic circuit. Therefore, by employing the structure described above, the quantity of material used for the rotor core can be reduced, and the inner diameter of the rotor can be increased up to a magnetically allowable position, and 20 accordingly the weight of the motor can be reduced.

In the above-mentioned structure, an effect different from the above-mentioned effect can be attained by changing a material forming the rotor core 7 from that of the stator core 4. For example, when an iron loss of the core in the 25 stator portion is large, a low iron-loss material is used for the stator core and a relatively higher iron-loss material is used for the rotor.

The relationship between saturation magnetic flux density and iron loss of a core is in a reversed relation, that is, a high iron-loss material has a high saturation magnetic flux density and a low iron-loss material has a 5 low saturation magnetic flux density. Therefore, it is possible to obtain a motor having a desired property by selecting which is required, high efficiency or small size.

In regard to solely the iron loss, the same effect described above can be obtained by changing the thickness 10 of the magnetic plates of the rotor core 7 and the stator core 4. The iron loss can be reduced by the thickness of the magnetic plates, but there are disadvantages in that number of the magnetic plates per core and number of the manufacturing processes are increased, and that the 15 mechanical strength of the core is decreased. Therefore, it is possible to obtain a high performance rotary electric machine by changing the thickness of the magnetic plates depending on necessity.

FIG. 4 shows a cross section in the direction 20 perpendicular to the shaft direction of another embodiment of a rotary electric machine in accordance with the present invention. This embodiment is an example of a reluctance motor having a rotor core with slits. Therein, parts having a similar function are identified by the reference 25 characters as in FIG. 1.

The rotor 3 is composed of a rotor core 7 formed of a magnetic body by laminating, for example, silicon steel

plates in the shaft direction and a rotor shaft 8. The rotor core 7 has a shape that a plurality of arc-shaped slits 72 are arranged concentrically in the circumferential direction with respect to a hole A as the center, and a 5 bridge 74 is concentrically arranged between the slits 72 in an arc shape similarly to the slits 72.

The bridges 74 are connected to each other in the peripheral portion with an outer peripheral bridge 71. That is, the rotor core has a structure capable of withstanding 10 the centrifugal force of the rotor 3 by the bridges to preventing the rotor core from being broken.

In this embodiment, the rotor core 7 is composed of projecting pole core portions 73 disposed in the outer peripheral side of the rotor core 7 and rotor core yoke 15 portions 76 forming magnetic flux paths of the projecting pole core portions 73, and the rotor core 7 is divided into six sections in the circumferential direction in the unit of the projecting pole core portion 73 and the rotor core yoke portion 76.

20 By the structure described above, the same advantages as in the structure shown by FIG. 1 can be displayed, and the eight of the rotor core 7 can be further reduced by existence of the slits 72.

FIG. 5 shows a cross section in the direction 25 perpendicular to the shaft direction of a further embodiment of a rotary electric machine in accordance with the present invention. This embodiment is an example of a

so-called permanent magnet rotary electric machine of an inner magnet type in which permanent magnets 6 are embeded in the rotor core 7.

As shown in FIG. 5, the stator 2 of the rotary electric machine 1 has completely the same structure as that in FIG. 1. On the other hand, the rotor is composed of a rotor core 7 formed of a magnetic body, for example, silicon steel plates and a rotor shaft 8. The rotor core 7 has permanent magnet inserting holes in which permanent magnets are inserted and placed. Further, projecting magnetic core portions 73 formed integrally with the rotor core 7 is arranged in both sides of the permanent magnets 6 in the circumferential direction.

In this embodiment is characterized by that the rotor core 7 is composed of the projecting magnetic pole core portion 73 placed in the outer peripheral side of the rotor core 7, the permanent magnets 6 contained in the rotor core 7 and the rotor core yoke portions 76 forming magnetic flux paths conducting in the projecting magnetic pole core portion 73 and the permanent magnets 6, and the rotor core 7 is divided into six sections in the circumferential direction in the unit of the projecting pole core portion 73 and the rotor core yoke portion 76.

Since the permanent magnet rotary electric machine of an inner magnet type having the above-described structure can use reluctance torque by the projecting pole core portion 73 as well as torque by the permanent magnets 6, a

high torque and high efficiency rotary electric machine can be obtained.

In this embodiment, the rotor 2 is formed of units of single pole, and the units of single pole are connected through the outer diameter bridges 71. Further, the units of single pole are assembled by being wound in one turn, and the dividing position of the rotor core 7 is selected at each of the projecting pole core portions 73 between the permanent magnets 6.

10 In this case, the rotor core 7 may be also divided in the unit of two magnetic poles or in the unit of three magnetic poles.

It can be suggested that the mechanical strength of the rotor 3 including the rotor core 7 may be decreased by 15 dividing the rotor core. Similarly to FIG. 1, the mechanical strength of the rotor core 7 can be reinforced by forming holes 11 at each position between the projecting pole core portion 73 and in the inner peripheral portion of the projecting pole core portion 73, and inserting an axial 20 direction fastening and supporting member 11a such as a rivet or a bolt into each of the holes 11 to fix the both ends of the axial direction fastening and supporting member 11a to both of side plates 12 of the rotor.

The weight of the rotor 3 can be reduced by placing a 25 solid boss (solid holding member having an I-shaped cross section) 13 in the inner periphery of the rotor core 7. Therefore, by employing the structure described above, the

quantity of material used for the rotor core can be reduced, and the weight of the motor can be reduced.

FIG. 6 shows one pole pair of another embodiment of a permanent magnet type rotary electric machine of three-phase 8-poles/48-slots in accordance with the present invention. Referring to FIG. 6, the structure of the stator 1 is the same as in a conventional stator, the stator 1 is formed by inserting and placing stator windings U1 for U-phase, stator windings V1 for V-phase and stator windings W1 for W-phase to 48 slots 3 formed in the nearly annular stator core 2. Opening portions 4 are formed corresponding to the slots in the inner periphery of the stator core.

On the other hand, the rotor 6 is constructed by press-fitting the rotor core, forming containing portions 15 formed by die-cut in the circumferential direction in the outer peripheral portion of the rotor core, and inserting permanent magnets 8 made of magnetized neodymium into the containing portions from the shaft direction so that the N-pole and the S-pole are alternatively arranged.

20 The rotor 6 is rotatably disposed in a state having a predetermined gap between the outer periphery of the rotor core 7 and the inner periphery of the stator core 2. The rotor core 7 is constructed by laminating many silicon steel plates which have holes for forming the containing 25 portions.

Let an inner radius of the rotor core 7 be  $\phi_1$ , a distance in the radial direction (a direction from the

shaft center of the rotor core toward the outer radius of the rotor core) from the inner diameter surface of the rotor core 7 to a side end portion between the poles of the inner peripheral surface of the permanent magnet 8 be  $r$ , 5 and a length of the permanent magnet in the circumferential direction be  $2 \cdot w$ . Therein, when the outer radius  $\phi_2$  of the rotor core 7 is constant, the value  $w$  becomes a constant value.

When the inner radius  $\phi_1$  of the rotor core 7 is 10 increased, that is, the value  $r$  is decreased, the weight of the motor (the rotor and the stator) is decreased since the amount of iron in the rotor is reduced.

FIG. 7 shows the relationship between ratio  $r/w$  and weight of the motor of the permanent magnet type rotary 15 electric machine of FIG. 6. The permanent magnet type rotary electric machine in this case is of 17 kW output, 187 mm outer diameter of the stator, 180 A input current and 160 V input voltage.

It can be understood from FIG. 7 that the motor 20 weight can be reduced by decreasing the ratio  $r/w$ . However, the magnetic fluxes of the permanent magnet become difficult to flow when the value  $r$  is too small.

FIG. 8 shows an analytical result of the magnetic field of the permanent magnet type rotary electric machine 25 of FIG. 6. Looking at the magnetic flux flow in the inner diameter side of the rotor 7 in FIG. 8, the magnetic fluxes flowing out from the surface of  $2 \cdot w$  length in the

circumferential direction of the permanent magnet 8 are divided into two flows of the magnetic fluxes each for width with respect to the boundary of magnet center to be respectively absorbed into the adjacent permanent magnets 8  
5 having the opposite polarity in the both sides.

When the distance  $r$  in the radial direction from the inner diameter surface of the rotor core 7 to a side end portion between the poles of the inner peripheral surface of the permanent magnet 8 is larger than the value  $w$ , that  
10 is,  $r/w > 1$ , the magnetic flux flow is smooth. However, when  $r/w < 1$ , the magnetic flux density in the gap 5 is decreased because the magnetic flux flow becomes uneven.

FIG. 9 shows the relationship between ratio  $r/w$  and magnetic flux density in the gap of the permanent magnet  
15 type rotary electric machine of FIG. 6. Referring to FIG. 9, the magnetic flux density  $B$  is nearly constant within the range of  $r/w > 0.8$ , but the magnetic flux density  $B$  rapidly decreases in  $r/w < 0.8$ . As the magnetic flux density  $B$  decreases, the output power of the motor is decreased.  
20 Since the laminating thickness of the cores must be increased in order to keep the output power constant, the motor weight is increased.

FIG. 10 shows the relationship between ratio  $r/w$  and motor weight of the permanent magnet type rotary electric  
25 machine of FIG. 6 under a condition of a constant output power. It can be understood from FIG. 10 that the motor weight can be reduced without decreasing the output power

of the motor when  $r/w \doteq 0.6 \pm 0.1$ . It is preferable that  $r/w \doteq 0.6$ .

The present invention can be applied not only to the case where the shape of the permanent magnet 8 is the arc-shape shown in the another embodiment, but also to cases of various shapes.

FIG. 11 shows one pole pair of another embodiment of a permanent magnet type rotary electric machine in accordance with the present invention in which the shape of the permanent magnet is rectangular. In this case, the shortest distance from the inner diameter surface of the rotor core 7 to the inner diameter surface of the permanent magnet 8 is a value  $s$  at the central portion of the magnet, but the characteristic of the motor is not changed even if the shortest distance is  $s$  because the magnetic fluxes flow toward the both sides. Similarly to the other embodiment, the characteristic changes depending on the distance  $r$  in the radial direction from the inner diameter surface of the rotor core 7 to a side end portion between the poles of the inner peripheral surface of the permanent magnet 8, and the condition to reducing the motor weight to minimum is  $r/w \doteq 0.6$ , also similarly to the case of the other embodiment.

FIG. 12 shows one pole pair of another embodiment of a permanent magnet type rotary electric machine in accordance with the present invention in which a plurality of die-cut holes 9 (magnetic gaps) are provided in the circumferential direction between the inner diameter

surface of the rotor core 7 and the inner peripheral surface of the permanent magnet 8.

In the case of FIG. 12, the severest condition for the magnetic flux flow is in the distance  $t$  in the radial direction from the permanent magnet 8 side of each of the die-cut holes 9 to the side end portion between the poles of the inner peripheral surface of each of the permanent magnets 8. The condition to reducing the motor weight to minimum is  $r/w \doteq 0.6$  because the same relationship as that in the other embodiments holds.

FIG. 13 shows a cross section in the direction perpendicular to the shaft direction of a further embodiment of a rotary electric machine in accordance with the present invention. This embodiment is an example of a rotary electric machine of an outer rotor with embedded magnet type. Therefore, the stator 2 and the rotor 3 of the rotary electric machine 1 are disposed oppositely to that of FIG. 1.

The stator 2 is a divided stator, and is disposed inside. On the other hand, the rotor 3 is composed of a rotor core 7 formed of a magnetic body by laminating, for example, silicon steel plates and a rotor case 15 made of a magnetic material. The rotor core 7 has permanent magnet inserting holes in which the permanent magnets 6 are inserted and placed. Further, projecting magnetic core portion 73 integrally formed with the rotor core 7 are arranged at the both sides of the permanent magnets 6 in

the circumferential direction.

The present embodiment is characterized by that the rotor is composed of the projecting magnetic core portions 73 arranged in the outer peripheral side of the rotor core 7, the permanent magnets 6 contained in the rotor core 7, and rotor core yoke portions 76 forming paths for magnetic fluxes passing through the projecting magnetic core portions 73 and the permanent magnets 6, and the rotor core 7 is divided into six sections in the circumferential direction in the unit of the projecting magnetic core portions 73 and the rotor core yoke portions 76.

Since the rotary electric machine of an outer rotor with embedded magnet type having the above-described structure can use reluctance torque by the projecting pole core portion 73 as well as torque by the permanent magnets 6, similarly to the rotary electric machine of FIG. 5, a high torque and high efficiency rotary electric machine can be obtained.

Further, the present embodiment is characterized by that the rotor 2 is formed of units of two poles. The units of two poles are connected through the outer diameter bridges 71, and the units of two poles are assembled by being wound in one turn. The dividing position of the rotor core 7 is selected at a position between the poles of the permanent magnets 6. The mechanical strength of the rotor 2 can be further increased by that in each of the dividing positions of the rotor core 7, the dividing position of

each of the magnetic plates composing the rotor core 7 laminated in the shaft direction are slightly displaced over other plates.

Particularly, in this embodiment, the rotor 2 is 5 divided in the unit of two poles and at the middle position of the width in the circumferential direction of the projecting pole core portion 73. Of course, it is possible to divide at middle position of the width in the circumferential direction of the permanent magnet 6.

10 The mechanical strength of the rotor core 7 in the outer rotor with embedded magnet structure is not so severe because it is supported by the rotor case 15. Therefore, number of the axial direction fastening and supporting members 11a such as rivets or bolts for the rotor core 7 15 can be reduced compared to the case of the inner rotor.

By the structure described above, the quantity of material used for the rotor core 7 can be reduced, and the weight of the rotary electric machine can be reduced.

Although the above embodiment describes on the rotary 20 electric machine of the lumped wound winding structure, the present embodiment may be applied to a rotary electric machine of the distributed wound winding structure. Further, the present invention may be applied to a motor or a generator.

25 Furthermore, the present embodiment may be applied both to a reluctance motor using an outer rotor type rotor and to a reluctance motor using an inner rotor type rotor.

The present embodiment may be applied not only to the rotary electric machines but also to a liner motor or the like.

An electric vehicle using an embodiment of the rotary electric machine in accordance with the present invention will be described below, referring to FIG. 14.

FIG. 14 is a schematic view showing the structure of a drive portion of an electric vehicle mounting an embodiment of the rotary electric machine in accordance with the present invention.

A car body of the electric vehicle is supported by four wheels 17, 18, 18, 20. Since the electric vehicle is of front wheel drive type, the embodiment of the rotary electric machine 1 in accordance with the present invention is directly attached to a front wheel shaft 25.

Driving torque of the rotary electric machine 1 is controlled by a controller 21. A battery 22 is provided as a power source for the controller 21, and electric power from the battery 22 is supplied to the rotary electric machine 1 through the controller 21, and the rotary electric machine 1 outputs drive torque, and then the wheels 17, 19 are rotated by the drive torque. Rotation of a steering wheel 23 is transmitted to the two wheels 17, 19 through a steering gear 24 and a transmitting mechanism composed of a tie rod, knuckle arms and so on to change an angle of the wheels.

By mounting the above-mentioned rotary electric

machine 1 on the electric vehicle, the vehicle can be made small in size and light in weight, and a driving distance per charge of the vehicle can be lengthened.

Although the above description is made on an example 5 of the electric vehicle, the same effect can be obtained by mounting the rotary electric machine 1 on a hybrid electric vehicle.

According to the present invention, by improving the material use factor at manufacturing the rotor core, 10 resources can be effectively used. Further, by making the rotary electric machine small in size and light in weight, the weight of the electric vehicle mounting the rotary electric machine can be reduced, and a driving distance per charge of the electric vehicle can be lengthened, and fuel 15 consuming efficiency can be improved.

Further, according to the present invention, the weight of the motor cab be reduced without decreasing the output power of the motor by making the rotary electric machine so as to satisfy the relation  $r/w \doteq 0.6 \pm 0.1$ , 20 where  $r$  is a distance in a radial direction from an inner radial surface of the rotor core to a side end portion between poles of an inner peripheral surface of each of the permanent magnets, and  $2w$  is a length in the circumferential direction of the permanent magnet.

25 Furthermore, by using the permanent magnet type rotary electric machine for a hybrid electric vehicle in accordance with the present invention, the weight of the

hybrid electric vehicle can be reduced.